## High-Dynamic-Range, Direct Upconversion 1500MHz to 2500MHz Quadrature Modulator


#### Abstract

General Description The MAX2022 low-noise, high-linearity, direct upconversion quadrature modulator is designed for single and multicarrier 1800 MHz to 2200 MHz UMTS/WCDMA, cdma2000®, and DCS/PCS base-station applications. Direct upconversion architectures are advantageous since they significantly reduce transmitter cost, part count, and power consumption as compared to traditional IF-based double upconversion systems. In addition to offering excellent linearity and noise performance, the MAX2022 also yields a high level of component integration. This device includes two matched passive mixers for modulating in-phase and quadrature signals, three LO mixer amplifier drivers, and an LO quadrature splitter. On-chip baluns are also integrated to allow for single-ended RF and LO connections. As an added feature, the baseband inputs have been matched to allow for direct interfacing to the transmit DAC, thereby eliminating the need for costly I/Q buffer amplifiers. The MAX2022 operates from a single +5 V supply. It is available in a compact 36-pin thin QFN package ( 6 mm $\times 6 \mathrm{~mm}$ ) with an exposed paddle. Electrical performance is guaranteed over the extended $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ temperature range.


## Applications

Single and Multicarrier WCDMA/UMTS Base Stations

Single and Multicarrier cdmaOne ${ }^{\text {TM }}$ and cdma2000 Base Stations
Single and Multicarrier DCS 1800/PCS 1900 EDGE Base Stations

PHS/PAS Base Stations
Predistortion Transmitters
Fixed Broadband Wireless Access
Wireless Local Loop
Private Mobile Radio
Military Systems
Microwave Links
Digital and Spread-Spectrum Communication Systems
cdma2000 is a registered trademark of Telecommunications Industry Association.
cdmaOne is a trademark of CDMA Development Group.

Features

- 1500 MHz to 2500 MHz RF Frequency Range
- Meets Four-Carrier WCDMA 65dBc ACLR
- +23.3dBm Typical OIP3
- +51.5 dBm Typical OIP2
- 45.7 dBc Typical Sideband Suppression
- -40dBm Typical LO Leakage
- -173.2dBm/Hz Typical Output Noise, Eliminating the Need for an RF Output Filter
- Broadband Baseband Input
- DC-Coupled Input Provides for Direct Launch DAC Interface, Eliminating the Need for Costly I/Q Buffer Amplifiers

Ordering Information

| PART | TEMP RANGE | PIN-PACKAGE | PKG <br> CODE |
| :---: | :---: | :---: | :---: |
| MAX2022ETX | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 36 Thin QFN-EP* <br> $(6 \mathrm{~mm} \times 6 \mathrm{~mm})$ | T3666-2 |
| MAX2022ETX-T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $36 \mathrm{Thin} \mathrm{QFN-EP}^{*}$ <br> $(6 \mathrm{~mm} \times 6 \mathrm{~mm})$ | T3666-2 |
| MAX2022ETX+D | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $36 \mathrm{Thin} \mathrm{QFN-EP*}$ <br> $(6 \mathrm{~mm} \times 6 \mathrm{~mm})$ | T3666-2 |
| MAX2022ETX+TD | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $36 \mathrm{Thin} \mathrm{QFN-EP*}$ <br> $(6 \mathrm{~mm} \times 6 \mathrm{~mm})$ | T3666-2 |

*EP = Exposed paddle. $\quad+=$ Lead free. $\quad D=$ Dry pack.
$-T=$ Tape-and-reel package.

WCDMA, ACLR, ALTCLR and Noise vs. RF Output Power at 2140MHz for Single, Two, and Four Carriers


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## ABSOLUTE MAXIMUM RATINGS



Note A: Maximum reliable continuous power applied to the baseband differential port is +12 dBm from an external $100 \Omega$ source.

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## DC ELECTRICAL CHARACTERISTICS

(MAX2022 Typical Application Circuit, $\mathrm{V} C \mathrm{C}=+4.75 \mathrm{~V}$ to +5.25 V , GND $=0 \mathrm{~V}$, I/Q inputs terminated into $100 \Omega$ differential, LO input terminated into $50 \Omega$, RF output terminated into $50 \Omega$, R1 $=432 \Omega$, R2 $=562 \Omega$, R3 $=301 \Omega, \mathrm{~T} \mathrm{C}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{V}_{\mathrm{CC}}=+5 \mathrm{~V}, \mathrm{~T}_{\mathrm{C}}=+25^{\circ} \mathrm{C}$, unless otherwise noted.) (Note 1)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNITS |
| :--- | :---: | :---: | ---: | :---: | :---: | :---: |
| Supply Voltage | $V_{C C}$ |  | 4.75 | 5.00 | 5.25 | V |
| Total Supply Current | ITOTAL | Pins 3, 13, 15, 31, 33 all connected to $\mathrm{V}_{\mathrm{CC}}$ | 292 | 342 | mA |  |
| Total Power Dissipation |  |  | 1460 | 1796 | mW |  |

## AC ELECTRICAL CHARACTERISTICS

(MAX2022 Typical Application Circuit, $\mathrm{V}_{C C}=+4.75 \mathrm{~V}$ to +5.25 V , GND $=0 \mathrm{~V}$, I/Q differential inputs driven from a $100 \Omega \mathrm{DC}$-coupled source, OV common-mode input, PLo $=0 \mathrm{dBm}, 1900 \mathrm{MHz} \leq \mathrm{fLO} \leq 2200 \mathrm{MHz}, 50 \Omega \mathrm{LO}$ and RF system impedance, R1 $=432 \Omega$, R2 = $562 \Omega$, $\mathrm{R} 3=301 \Omega, \mathrm{~T}_{\mathrm{C}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. Typical values are at $\mathrm{V}_{\mathrm{CC}}=+5 \mathrm{~V}, \mathrm{~V}_{\mathrm{BBI}}=109 \mathrm{~m} \mathrm{~V}_{\mathrm{P}-\mathrm{P}}$ differential, $\mathrm{V}_{\mathrm{BBQ}}=109 \mathrm{~m} \mathrm{~V}_{\mathrm{P}-\mathrm{P}}$ differential, $\mathrm{f}_{\mathrm{I}} \mathrm{Q}=1 \mathrm{MHz}, \mathrm{T} \mathrm{C}=+25^{\circ} \mathrm{C}$, unless otherwise noted.) (Note 1)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BASEBAND INPUT |  |  |  |  |  |  |
| Baseband Input Differential Impedance |  | $\mathrm{f}_{\mathrm{I}} \mathrm{Q}=1 \mathrm{MHz}$ |  | 43 |  | $\Omega$ |
| BB Common-Mode Input Voltage Range |  |  | -2.5 | 0 | +1.5 | V |
| Output Power |  | $\mathrm{T}_{\mathrm{C}}=+25^{\circ} \mathrm{C}$ | -24 |  |  | dBm |
| RF OUTPUTS (fLO = 1960MHz) |  |  |  |  |  |  |
| Output IP3 |  | $\mathrm{V}_{\mathrm{BBI}}, \mathrm{V}_{\mathrm{BBQ}}=547 \mathrm{~m} \mathrm{~V}_{\text {P-P }}$ differential per tone into $50 \Omega$, $\begin{aligned} & \mathrm{f}_{\mathrm{BB} 1}=1.8 \mathrm{MHz}, \\ & \mathrm{f}_{\mathrm{BB} 2}=1.9 \mathrm{MHz} \end{aligned}$ |  | 21.8 |  | dBm |
| Output IP2 |  | $\mathrm{V}_{\mathrm{BBI}}, \mathrm{V}_{\mathrm{BBQ}}=547 \mathrm{~m} \mathrm{~V}_{\text {P-P }}$ differential per tone into $50 \Omega$, <br> $\mathrm{f}_{\mathrm{BB}} 1=1.8 \mathrm{MHz}$, <br> $\mathrm{f}_{\mathrm{BB} 2}=1.9 \mathrm{MHz}$ |  | 48.9 |  | dBm |
| Output Power |  |  |  | -20.5 |  | dBm |

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## AC ELECTRICAL CHARACTERISTICS (continued)

(MAX2022 Typical Application Circuit, $\mathrm{V} C \mathrm{C}=+4.75 \mathrm{~V}$ to +5.25 V , GND $=0 \mathrm{~V}$, I/Q differential inputs driven from a $100 \Omega \mathrm{DC}$-coupled source, OV common-mode input, PLo $=0 \mathrm{dBm}, 1900 \mathrm{MHz} \leq f \mathrm{fo} \leq 2200 \mathrm{MHz}, 50 \Omega \mathrm{LO}$ and RF system impedance, R1 $=432 \Omega$, R2 $=$ $562 \Omega, R 3=301 \Omega, \mathrm{~T}_{\mathrm{C}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. Typical values are at $\mathrm{V}_{\mathrm{CC}}=+5 \mathrm{~V}, \mathrm{~V}_{\mathrm{BBI}}=109 \mathrm{mV}$ P-P differential, $\mathrm{V}_{\mathrm{BBQ}}=109 \mathrm{mV}$ P-p differential, $\mathrm{f}_{\mathrm{Q}}=1 \mathrm{MHz}, \mathrm{TC}=+25^{\circ} \mathrm{C}$, unless otherwise noted.) (Note 1)


Note 1: $T_{C}$ is the temperature on the exposed paddle.
Note 2: Single-carrier WCDMA peak-to-average ratio of 10.5 dB for $0.1 \%$ complimentary cumulative distribution function.

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$\qquad$
(MAX2022 Typical Application Circuit, $50 \Omega$ LO input, R1 $=432 \Omega$, R2 $=562 \Omega, \mathrm{R} 3=301 \Omega, \mathrm{~V}_{\mathrm{CC}}=+5 \mathrm{~V}, \mathrm{PLO}=0 \mathrm{dBm}, \mathrm{V}_{\mathrm{IFI}}=\mathrm{V}_{\mathrm{IFQ}}=$ 109 mV P-p differential, $\mathrm{f}_{\mathrm{I} Q}=1 \mathrm{MHz}, \mathrm{I} / \mathrm{Q}$ differential inputs driven from a $100 \Omega \mathrm{DC}$-coupled source, common-mode input from $0 \mathrm{~V}, \mathrm{~T}_{\mathrm{C}}=$ $+25^{\circ} \mathrm{C}$, unless otherwise noted.)





OUTPUT POWER vs. LO FREQUENCY


LO LEAKAGE vs. LO FREQUENCY


ACLR vs. OUTPUT POWER


OUTPUT POWER vs. LO FREQUENCY


LO LEAKAGE vs. LO FREQUENCY


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## Typical Operating Characteristics (continued)

(MAX2022 Typical Application Circuit, $50 \Omega \mathrm{LO}$ input, $\mathrm{R} 1=432 \Omega$, $\mathrm{R} 2=562 \Omega, \mathrm{R} 3=301 \Omega, \mathrm{~V}_{\mathrm{CC}}=+5 \mathrm{~V}, \mathrm{PLO}=0 \mathrm{dBm}, \mathrm{V}_{\mathrm{IFI}}=\mathrm{V}_{\mathrm{IFQ}}=$ 109 mV P-p differential, $\mathrm{f}_{\mathrm{IQ}}=1 \mathrm{MHz}$, I/Q differential inputs driven from a $100 \Omega \mathrm{DC}$-coupled source, common-mode input from $0 \mathrm{~V}, \mathrm{TC}=$ $+25^{\circ} \mathrm{C}$, unless otherwise noted.)


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(MAX2022 Typical Application Circuit, $50 \Omega$ LO input, $\mathrm{R} 1=432 \Omega$, R2 $=562 \Omega, \mathrm{R} 3=301 \Omega, \mathrm{~V}_{\mathrm{CC}}=+5 \mathrm{~V}, \mathrm{PLO}=0 \mathrm{dBm}, \mathrm{V}_{\mathrm{IFI}}=\mathrm{V}_{\mathrm{IFQ}}=$ 109 mV P-P differential, $\mathrm{f}_{\mathrm{IQ}}=1 \mathrm{MHz}, \mathrm{I} / \mathrm{Q}$ differential inputs driven from a $100 \Omega \mathrm{DC}$-coupled source, common-mode input from $0 \mathrm{~V}, \mathrm{~T}_{\mathrm{C}}=$ $+25^{\circ} \mathrm{C}$, unless otherwise noted.)

vs. COMMON-MODE BASEBAND VOLTAGE


OUTPUT IP2
vs. 10 FREQUENCY



OUTPUT IP2
vs. LO FREQUENCY


OUTPUT IP2
vs. COMMON-MODE BASEBAND VOLTAGE


OUTPUT IP3 vs. 10 FREQUENCY


OUTPUT IP2
vs. 10 FREQUENCY


LO LEAKAGE vs. LO FREQUENCY


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## Typical Operating Characteristics (continued)

(MAX2022 Typical Application Circuit, $50 \Omega$ LO input, R1 $=432 \Omega$, R2 $=562 \Omega, \mathrm{R} 3=301 \Omega, \mathrm{~V}_{\mathrm{CC}}=+5 \mathrm{~V}, \mathrm{P} \mathrm{LO}=0 \mathrm{dBm}, \mathrm{V}_{\mathrm{IFI}}=\mathrm{V}_{\mathrm{IFQ}}=$ 109 mV P-p differential, $\mathrm{f} / \mathrm{Q}=1 \mathrm{MHz}$, $\mathrm{I} / \mathrm{Q}$ differential inputs driven from a $100 \Omega \mathrm{DC}$-coupled source, common-mode input from $\mathrm{OV}, \mathrm{T} \mathrm{C}=$ $+25^{\circ} \mathrm{C}$, unless otherwise noted.)


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## Typical Operating Characteristics (continued)

(MAX2022 Typical Application Circuit, $50 \Omega$ LO input, R1 $=432 \Omega$, R2 $=562 \Omega, \mathrm{R} 3=301 \Omega, \mathrm{~V}_{\mathrm{CC}}=+5 \mathrm{~V}, \mathrm{PLO}=0 \mathrm{dBm}, \mathrm{V}_{\mathrm{IFI}}=\mathrm{V}_{\mathrm{IFQ}}=$ 109 mV P-P differential, $\mathrm{f}_{\mathrm{IQ}}=1 \mathrm{MHz}$, I/Q differential inputs driven from a $100 \Omega \mathrm{DC}$-coupled source, common-mode input from $0 \mathrm{~V}, \mathrm{~T} \mathrm{C}=$ $+25^{\circ} \mathrm{C}$, unless otherwise noted.)


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Pin Description

| PIN | NAME |  |
| :---: | :---: | :--- |
| $1,5,9-12,14$, <br> $16-19,22,24$, <br> $27-30,32,34$, <br> 35,36 | GND | GUNCTION |
| 2 | RBIASLO3 | 3rd LO Amplifier Bias. Connect a 301 $\Omega$ resistor to ground. |
| 3 | VCCLOA | LO Input Buffer Amplifier Supply Voltage |
| 4 | LO | Local Oscillator Input. 50 $\Omega$ input impedance. |
| 6 | RBIASLO1 | 1st LO Input Buffer Amplifier Bias. Connect a 432ת resistor to ground. |
| 7 | COMP | Compensation Capacitor Input. Connect a 22pF capacitor to ground. |
| 8 | RBIASLO2 | 2nd LO Amplifier Bias. Connect a 562』 resistor to ground. |
| 13 | VCCLOI1 | I-Channel 1st LO Amplifier Supply Voltage |
| 15 | VCCLOI2 | I-Channel 2nd LO Amplifier Supply Voltage |
| 20 | BBIP | Baseband In-Phase Positive Input |
| 21 | BBIN | Baseband In-Phase Negative Input |
| 23 | RFOUT | RF Output |
| 25 | BBQN | Baseband Quadrature Negative Input |
| 26 | BBQP | Baseband Quadrature Positive Input |
| 31 | VCCLOQ2 | Q-Channel 1st LO Amplifier Supply Voltage |
| 33 | VCCLOQ1 | Q-Channel 2nd LO Amplifier Supply Voltage |
| EP | GND | Exposed Ground Paddle. The exposed paddle MUST be soldered to the ground plane using <br> multiple vias. |

## Detailed Description

The MAX2022 is designed for upconverting differential in-phase (I) and quadrature (Q) inputs from baseband to a 1500 MHz to 2500 MHz RF frequency range. Applications include single and multicarrier 1800 MHz to 2200MHz UMTS/WCDMA, cdma2000, and DCS/PCS base stations. Direct upconversion architectures are advantageous since they significantly reduce transmitter cost, part count, and power consumption as compared to traditional IF-based double upconversion systems.
The MAX2022 integrates internal baluns, an LO buffer, a phase splitter, two LO driver amplifiers, two matched double-balanced passive mixers, and a wideband quadrature combiner. Precision matching between the in-phase and quadrature channels, and highly linear mixers achieves excellent dynamic range, ACLR, 1dB compression point, and LO and sideband suppression, making it ideal for four-carrier WCDMA/UMTS operation.

## LO Input Balun, LO Buffer, and Phase Splitter

The MAX2022 requires a single-ended LO input, with a nominal power of 0 dBm . An internal low-loss balun at
the LO input converts the single-ended LO signal to a differential signal at the LO buffer input. In addition, the internal balun matches the buffer's input impedance to $50 \Omega$ over the entire band of operation.
The output of the LO buffer goes through a phase splitter, which generates a second LO signal that is shifted by $90^{\circ}$ with respect to the original. The $0^{\circ}$ and $90^{\circ} \mathrm{LO}$ signals drive the I and Q mixers, respectively.

## LO Driver

Following the phase splitter, the $0^{\circ}$ and $90^{\circ} \mathrm{LO}$ signals are each amplified by a two-stage amplifier to drive the I and Q mixers. The amplifier boosts the level of the LO signals to compensate for any changes in LO drive levels. The two-stage LO amplifier allows a wide input power range for the LO drive. While a nominal LO power of OdBm is specified, the MAX2022 can tolerate LO level swings from -3 dBm to +3 dBm .

## I/Q Modulator

The MAX2022 modulator is composed of a pair of matched double-balanced passive mixers and a balun. The I and Q differential baseband inputs accept signals from DC to beyond 100 MHz with differential amplitudes

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up to $2 \mathrm{~V}_{\mathrm{P}-\mathrm{P}}$ differential (common-mode input equals 0 V ). The wide input bandwidth allows for direct interface with the baseband DACs. No active buffer circuitry between the baseband DAC and the MAX2022 is required.
The I and Q signals directly modulate the $0^{\circ}$ and $90^{\circ}$ LO signals and are upconverted to the RF frequency. The outputs of the I and $Q$ mixers are combined through a balun to a singled-ended RF output.

## Applications Information

## LO Input Drive

The LO input of the MAX2022 requires a single-ended drive at a 1500 MHz to 2500 MHz frequency. It is internally matched to $50 \Omega$. An integrated balun converts the singled-ended input signal to a differential signal at the LO buffer differential input. An external DC-blocking capacitor is the only external part required at this interface. The LO input power should be within the -3 dBm to +3 dBm range.

COMP Pin
The COMP pin is used to provide additional lowpass filtering to the bias circuit noise. An external capacitor can be used from the COMP pin to ground to reduce the close-in noise of the modulator. For UMTS, connecting a 22 pF capacitor from the COMP pin to ground is recommended to filter out noise and frequency offsets
above 3.5 MHz . For GSM, connecting a 1 nF capacitor from COMP to ground is recommended for filtering out noise and frequency offsets above 600 kHz .

Baseband I/Q Input Drive
The MAX2022 I and Q baseband inputs should be driven differentially for best performance. The baseband inputs have a $50 \Omega$ differential input impedance. The optimum source impedance for the I and Q inputs is $100 \Omega$ differential. This source impedance will achieve the optimal signal transfer to the I and $Q$ inputs, and the optimum output RF impedance match. The MAX2022 can accept input power levels of up to +12 dBm on the I and $Q$ inputs. Operation with complex waveforms, such as CDMA or WCDMA carriers, utilize input power levels that are far lower. This lower power operation is made necessary by the high peak-to-average ratios of these complex waveforms. The peak signals must be kept below the compression level of the MAX2022. The input common-mode voltage should be confined to the -2 V to +1.5V DC range.
The MAX2022 is designed to interface directly with Maxim high-speed DACs. This generates an ideal total transmitter lineup, with minimal ancillary circuit elements. Such DACs include the MAX5875 series of dual DACs, and the MAX5895 dual interpolating DAC. These DACs have ground-referenced differential current outputs. Typical termination of each DAC output into a $50 \Omega$ load


Figure 1. MAX5895 DAC Interfaced with MAX2022

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resistor to ground, and a 10 mA nominal DC output current results in a 0.5 V common-mode DC level into the modulator I/Q inputs. The nominal signal level provided by the DACs will be in the -12 dBm range for a single CDMA or WCDMA carrier, reducing to -18 dBm per carrier for a four-carrier application.
The I/Q input bandwidth is greater than 50 MHz at -0.1 dB response. The direct connection of the DAC to the MAX2022 insures the maximum signal fidelity, with no performance-limiting baseband amplifiers required. The DAC output can be passed through a lowpass filter to remove the image frequencies from the DAC's output response. The MAX5895 dual interpolating DAC can be operated at interpolation rates up to $\times 8$. This has the benefit of moving the DAC image frequencies to a very high, remote frequency, easing the design of the baseband filters. The DAC's output noise floor and interpolation filter stopband attenuation are sufficiently good to insure that the 3GPP noise floor requirement is met for large frequency offsets, 60 MHz for example, with no filtering required on the RF output of the modulator.
Figure 1 illustrates the ease and efficiency of interfacing the MAX2022 with a Maxim DAC, in this case the MAX5895 dual 16-bit interpolating-modulating DAC.
The MAX5895 DAC has programmable gain and differential offset controls built in. These can be used to optimize the LO leakage and sideband suppression of the MAX2022 quadrature modulator.

## RF Output

The MAX2022 utilizes an internal passive mixer architecture. This enables a very low noise floor of $-173.2 \mathrm{dBm} / \mathrm{Hz}$ for low-level signals, below about
-20dBm output power level. For higher output level signals, the noise floor will be determined by the internal LO noise level at approximately $-162 \mathrm{dBc} / \mathrm{Hz}$.
The I/Q input power levels and the insertion loss of the device will determine the RF output power level. The input power is the function of the delivered input I and $Q$ voltages to the internal $50 \Omega$ termination. For simple sinusoidal baseband signals, a level of 89 mVP -p differential on the I and the Q inputs results in an input power level of -17 dBm delivered to the I and Q internal $50 \Omega$ terminations. This results in a -27 dBm RF output power.

## Generation of WCDMA Carriers

The MAX2022 quadrature modulator makes an ideal signal source for the generation of multiple WCDMA carriers. The combination of high OIP3 and exceptionally low output noise floor gives an unprecedented output dynamic range. The output dynamic range allows the generation of four WCDMA carriers in the UMTS band with a noise floor sufficiently low to meet the 3GPP specification requirements with no additional RF filtering. This promotes an extremely simple and efficient transmitter lineup. Figure 2 illustrates a complete transmitter lineup for a multicarrier WCDMA transmitter in the UMTS band.
The MAX5895 dual interpolating-modulating DAC is operated as a baseband signal generator. For generation of four carriers of WCDMA modulation, and digital predistortion, an input data rate of 61.44 or 122.88 Mbps can be used. The DAC can then be programmed to operate in $\times 8$ or $\times 4$ interpolation mode, resulting in a 491.52Msps output sample rate. The DAC will generate four carriers of WCDMA modulation


Figure 2. Complete Transmitter Lineup for a Multicarrier WCDMA in the UMTS Band

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with an ACLR typically greater than 77 dB under these conditions. The output power will be approximately -18 dBm per carrier, with a noise floor typically less than $-144 \mathrm{dBc} / \mathrm{Hz}$.
The MAX5895 DAC has built-in gain and offset fine adjustments. These are programmable by a 3 -wire serial logic interface. The gain adjustment can be used to adjust the relative gains of the I and Q DAC outputs. This feature can be used to improve the native sideband suppression of the MAX2022 quadrature modulator. The gain adjustment resolution of 0.01 dB allows sideband nulling down to approximately -60dB. The offset adjustment can similarly be used to adjust the offset DC output of each I and Q DAC. These offsets can then be used to improve the native LO leakage of the MAX2022. The DAC resolution of 4 LSBs will yield nulled LO leakage of typically less than -50 dBc relative to four-carrier output levels.
The DAC outputs must be filtered by baseband filters to remove the image frequency signal components. The baseband signals for four-carrier operation cover DC to 10 MHz . The image frequency appears at 481 MHz to 491 MHz . This very large frequency spread allows the use of very low-complexity lowpass filters, with excellent in-band gain and phase performance. The low DAC noise floor allows for the use of a very wideband filter, since the filter is not necessary to meet the 3GPP noise floor specification.
The MAX2022 quadrature modulator then upconverts the baseband signals to the RF output frequency. The output power of the MAX2022 will be approximately -28 dBm per carrier. The noise floor will be less than $-169 \mathrm{dBm} / \mathrm{Hz}$, with an ACLR typically greater than 65dBc. This performance meets the 3GPP specification requirements with substantial margins. The noise floor performance will be maintained for large offset frequencies, eliminating the need for subsequent RF filtering in the transmitter lineup.
The RF output from the MAX2022 is then amplified by a combination of a low-noise amplifier followed by a MAX2057 RF-VGA. This VGA can be used for lineup compensation for gain variance of transmitter and power amplifier elements. No significant degradation of the signal or noise levels will be incurred by this additional amplification. The MAX2057 will deliver an output
power of -6 dBm per carrier, 0 dBm total at an ACLR of 65 dB and noise floor of $-142 \mathrm{dBc} / \mathrm{Hz}$.

## Layout Considerations

A properly designed PC board is an essential part of any RF/microwave circuit. Keep RF signal lines as short as possible to reduce losses, radiation, and inductance. For the best performance, route the ground pin traces directly to the exposed pad under the package. The PC board exposed paddle MUST be connected to the ground plane of the PC board. It is suggested that multiple vias be used to connect this pad to the lowerlevel ground planes. This method provides a good RF/thermal conduction path for the device. Solder the exposed pad on the bottom of the device package to the PC board. The MAX2022 evaluation kit can be used as a reference for board layout. Gerber files are available upon request at www.maxim-ic.com.

Power-Supply Bypassing Proper voltage-supply bypassing is essential for highfrequency circuit stability. Bypass all Vcc pins with 22 pF and $0.1 \mu \mathrm{~F}$ capacitors placed as close to the pins as possible. The smallest capacitor should be placed closest to the device.
To achieve optimum performance, use good voltagesupply layout techniques. The MAX2022 has several RF processing stages that use the various VCC pins, and while they have on-chip decoupling, off-chip interaction between them may degrade gain, linearity, carrier suppression, and output power-control range. Excessive coupling between stages may degrade stability.

## Exposed Pad RF/Thermal Considerations

 The EP of the MAX2022's 36 -pin thin QFN-EP package provides a low thermal-resistance path to the die. It is important that the PC board on which the IC is mounted be designed to conduct heat from this contact. In addition, the EP provides a low-inductance RF ground path for the device.The exposed paddle (EP) MUST be soldered to a ground plane on the PC board either directly or through an array of plated via holes. An array of 9 vias, in a $3 \times$ 3 array, is suggested. Soldering the pad to ground is critical for efficient heat transfer. Use a solid ground plane wherever possible.

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Table 1. Component List Referring to the Typical Application Circuit

| COMPONENT | VALUE | DESCRIPTION |
| :---: | :---: | :--- |
| C1, C3, C4, C6, C7, C10, C13 | 22 pF | $22 \mathrm{pF} \pm 5 \%, 50 \mathrm{~V}$ C0G ceramic capacitors (0402) |
| $\mathrm{C} 2, \mathrm{C} 5, \mathrm{C} 8, \mathrm{C} 11, \mathrm{C} 12$ | $0.1 \mu \mathrm{~F}$ | $0.1 \mu \mathrm{~F} \pm 10 \%, 16 \mathrm{~V}$ XR ceramic capacitors (0603) |
| C9 | 1.2 pF | $1.2 \mathrm{pF} \pm 0.1 \mathrm{pF}, 50 \mathrm{~V}$ C0G ceramic capacitor (0402) |
| R1 | $432 \Omega$ | $432 \Omega \pm 1 \%$ resistor (0402) |
| R2 | $562 \Omega$ | $562 \Omega \pm 1 \%$ resistor (0402) |
| R3 | $301 \Omega$ | $301 \Omega \pm 1 \%$ resistor (0402) |



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